

## ESCAN

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## Outline

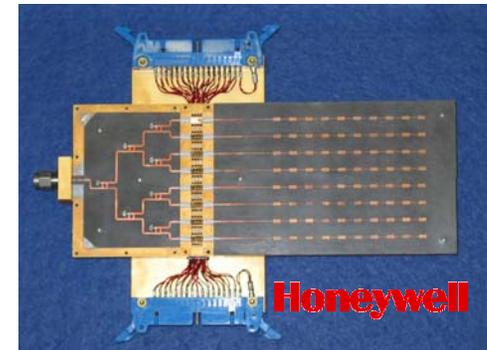
- **Reconfigurable Antennas**
  - Nomenclature... What is Reconfigurable?
  - Benefits
- **ESCAN**
  - Design
  - Program Goals
  - ASIC Development
    - RF Switch Performance
    - Photocell Performance
  - Required Steps in Array Fabrication & Measurement

## Reconfigurable Array

- Reconfigurable apertures are distinguished from other types of traditional electronic antennas by their ability to alter the current distribution through their aperture. A reconfigurable array is capable of changing its element pattern and complex array factor.<sup>1</sup>

Fixed element pattern of Phased Array →

$$\vec{E} = \frac{j\omega\mu_0 e^{-jk\vec{r}_o}}{\vec{r}_o} f_e(\theta, \phi) \sum_1^N a_i e^{-jk(\hat{r}\cdot\vec{r}_i)}$$



Electronically Steered Phased Array

Reconfigurable Element Pattern

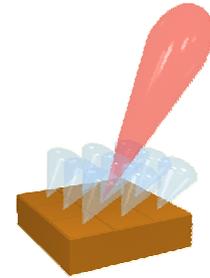
$$\vec{E} = \frac{j\omega\mu_0 e^{-jk\vec{r}_o}}{\vec{r}_o} \sum_1^N f_i(\theta, \phi) a_i e^{-jk(\hat{r}\cdot\vec{r}_i)}$$

## Basic Features of Reconfigurable Elements

- **A Structural Design that Enables the Radiator to Electrically Evolve**
  - High capacity to vary element shape and resonant length scales
    - Antennas that switch a limited number of radiators in and out are often referred to as “Smart or Adaptive” and have more restricted performance
  - A design which allows for broadband impedance matching capability
    - Maximizes bandwidth and gain
    - Improves beam steering capability with a single feed
- **Embedded Control Electronics**
  - Deliver power and reconfiguration instruction into the aperture
  - Minimize electromagnetic interference with the radiative function (no conductive wires)
  - Maintain the current distribution integrity through the aperture
  - Enable fast reconfiguration times
    - Facilitates tracking

## Benefits of Reconfigurable Elements/Arrays

- **Multifunctional Aperture**
  - Possesses weight, cost, and signature reduction benefits
- **Adapts to the External Communication Environment**
  - Null steering for anti-jamming capability
  - Enables gain for bandwidth trades
- **Single Feed Steering**
  - Reconfigurable structures permit steering at frequencies above the grating lobes without the immediate loss in gain experienced in phased array concepts.
- **Low Observables**
  - During periods when the antenna functionality is not required the reconfigurability of the aperture may be utilized to force the structure to function as R-card for signature reduction.



Reconfigurable  
Aperture

## ESCAN: 800MHz-2.6GHz 5x1 Reconfigurable Array

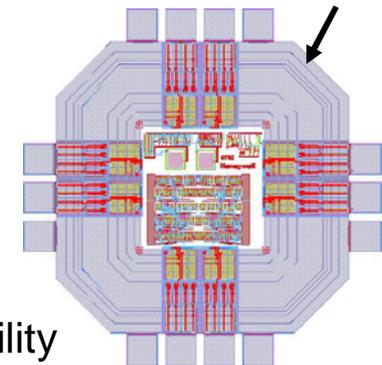
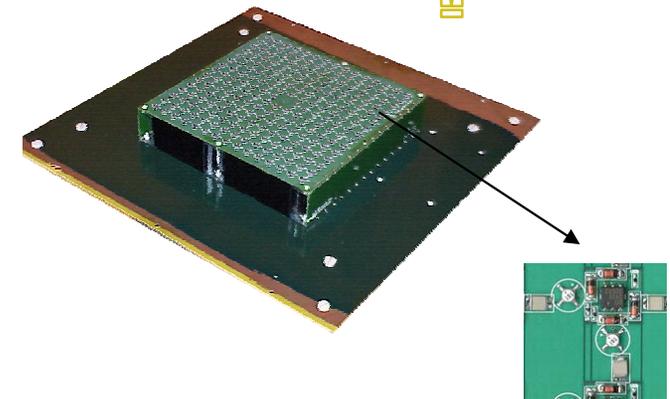
- **Structural Form of the Element**

- Utilizes a proven reconfigurable element concept developed at Georgia Tech (GTRI)<sup>2</sup>
- Funded by DARPA RECAP/ FCS-C Programs
  - **GTRI RECAP** Bandwidth: 500MHz-2.7GHz
  - **GTRI RECAP** Directive Gain: 14dB ( $1.3\lambda \times 1.3\lambda$ )
  - **GTRI RECAP** Beamsteer:  $\pm 55^\circ$

- **Embedded Control Electronics**

- Utilizes a Honeywell electronics design solely driven by an optical interface
  - Optical backplane is composed of DSP controlled VCSEL array
  - ASIC development for the embedded aperture electronics
  - Power efficient economical solution with improved manufacturability

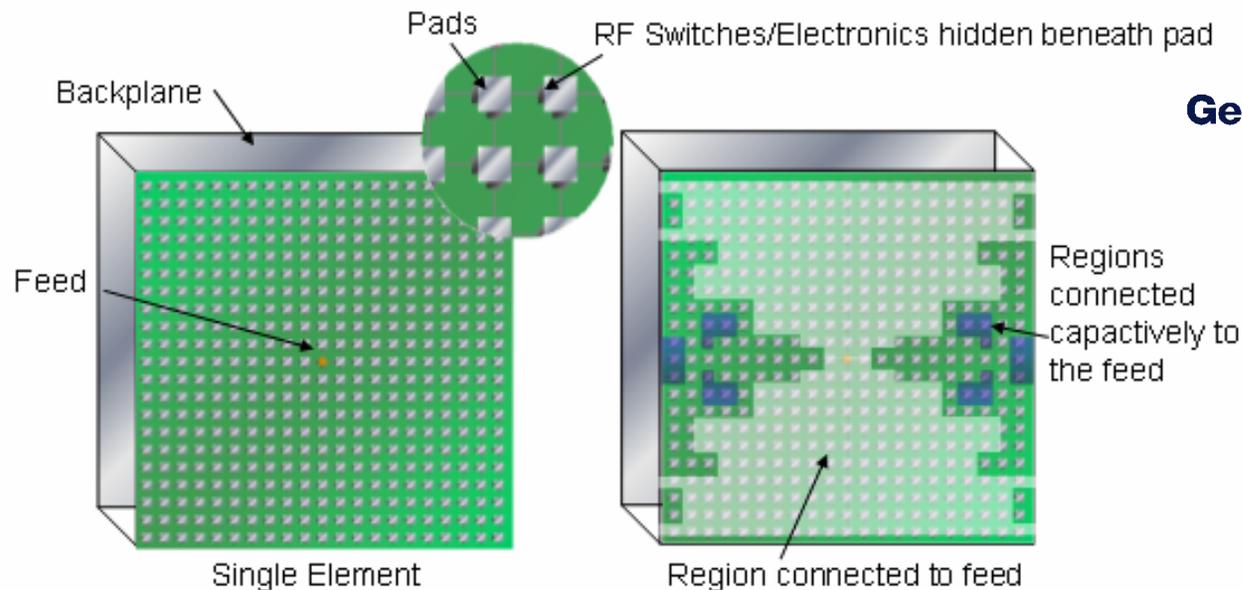
Georgia Tech  
Research Institute



1.J. C. Maloney, M.P. Kesler, L. M. Lust, L.N. Pringle, T. L. Fountain, P. H. Harms, G.S. Smith,  
" Switched Fragmented Aperture Antennas", IEEE Antennas Propagat. Soc. Int. Symposium., vol 1, pp. 310-313, July 2000.

## ESCAN's Structural Form is Based on GTRI RECAP

- The radiative pattern generated from a single feed element may be reconfigured by connective switches located between each pad.
  - Individual pads  $\ll \lambda$  and are not resonate alone
  - Collectively the pads connected to the feed generate a radiating form.
  - The parasitic pads capacitively coupled to the feed may be configured to improve matching characteristics enabling wider band performance.

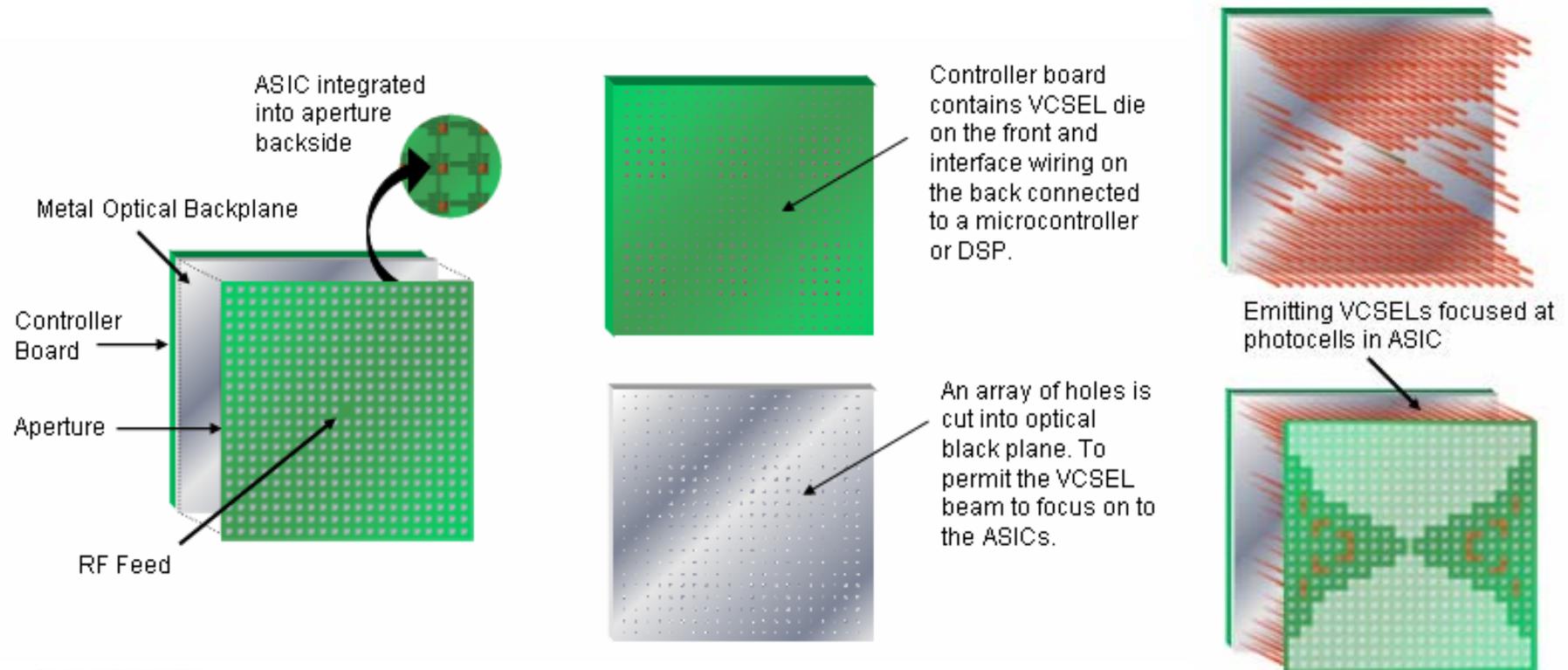


## ESCAN: Design Rules of Thumb for the Structural Architecture

- **Pad Dimension: 1cm**
- **Pad Density  $\lambda/7$  to  $\lambda/11$** 
  - Increased density permits broader beamsteering but forces higher switch density into the aperture.
- **Element Dimension  $2\lambda \times 2\lambda$  ( 25cm x 25cm)**
  - 20 x 20 pads (400 pads/element)
- **Array Dimension 5x1 (1.25m x 0.25m)**
- **Ground Plane Distance  $\lambda/4$  @ 2.4 GHz (3cm)**

## ESCAN: Honeywell's Embedded Controls

- Power efficiency enables pure optical interface
  - ASIC embedded behind each pad contains a photocell and RF switch
  - VCSEL array is situated on a PCB behind the antenna ground plane
  - VCSEL array is controlled by 1 DSP/microcontroller per element

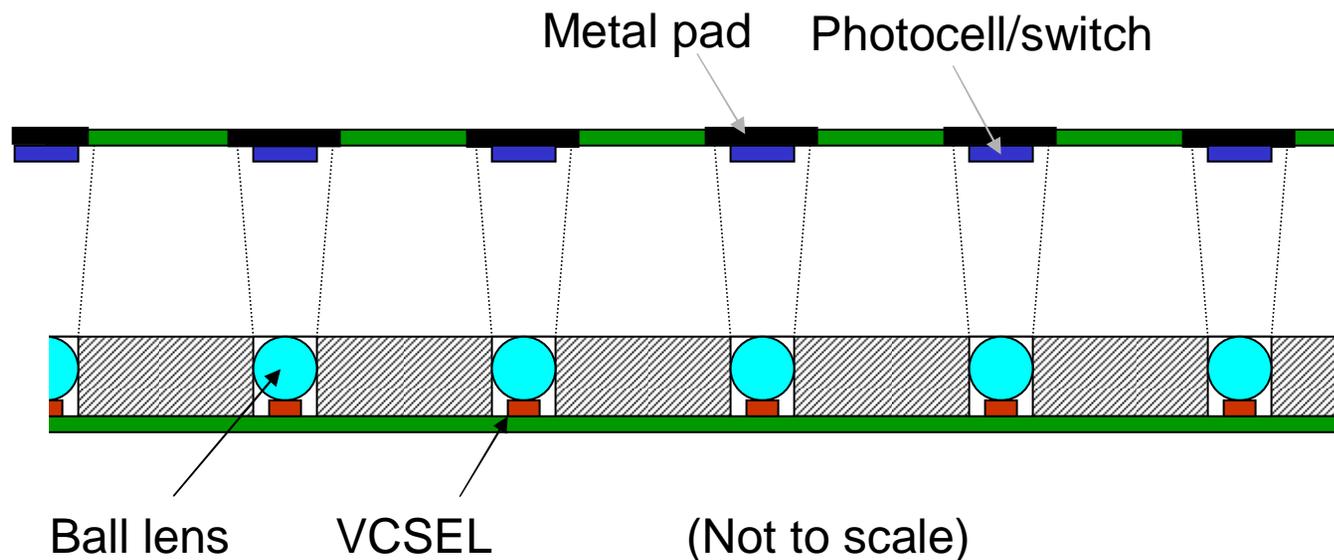


## ESCAN Program Goals

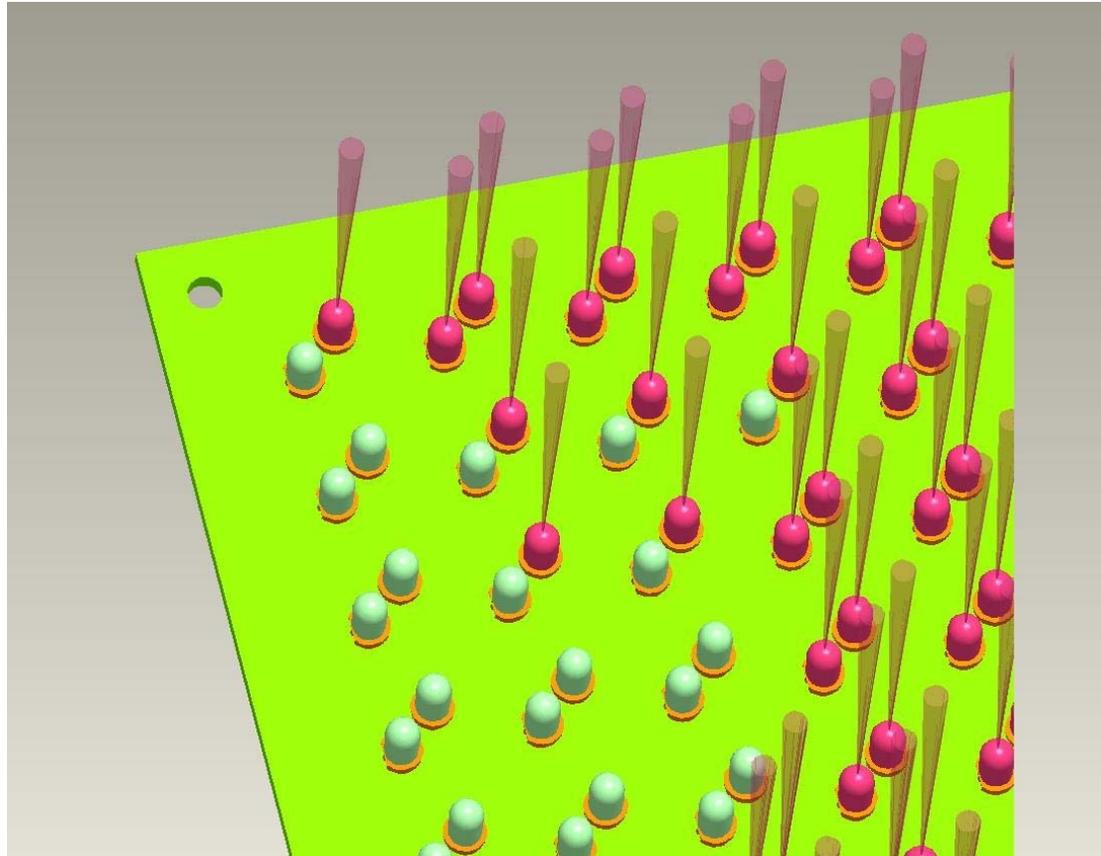
- **Bandwidth: 800MHz -2.6GHz**
- **Element Broadside Gain: 13dB @ 2.4GHz and 7dB @ 900Mhz**
  - Theoretical Aperture Gain= $4A\pi/\lambda^2=17\text{dB}$
- **5 x 1 Array Broadside Gain: 19dB @ 2.4GHz and 13dB @ 900Mhz**
- **Element Broadside Beamwidth: 32deg @ 2.4GHz 85deg @ 900MHz**
- **Array Broadside Beamwidth: 4.5deg @ 2.4GHz 12deg @ 900MHz**
- **Steering: +/-70 deg**
  - Controlled by pad density and the insertion form factor of the array
- **Power Handling: 1W CW per feed at 2.4GHz**
  - Switch dependent
- **Reconfiguration Time: 20 usec**
  - Dependent on photocell
- **Production cost: \$3K-\$5K/element**
- **Ease of Manufacture**

## ESCAN ASIC Development

- ASIC includes 2 RF switches and photodetector (PD)
- Switch insertion loss needs to be minimized and isolation maximized for good power handling and antenna gain
- VCSEL output is concentrated on photocell array to maximize photocurrent and switching speed



## VCSEL Switch Control Subsystem



## ESCAN VCSEL & Photocell Considerations

- **Honeywell Designed VCSEL SV5637-001**
  - 850nm wavelength
  - Beam divergence ~ 2 degrees
  - 1.1 mm spot diameter at photovoltaic cell
  - Output power 1.5 mW

### • **11 Cell GaAs Process**

- Photovoltaic cell area 11 x 0.25 mm<sup>2</sup>
- Power received ~136  $\mu$ W
- $10^{17}$  n-doping photovoltaic cell (92 pF, ~68  $\mu$ A photocurrent @ ~0.8volts)
- Switching time ~ 1  $\mu$ s

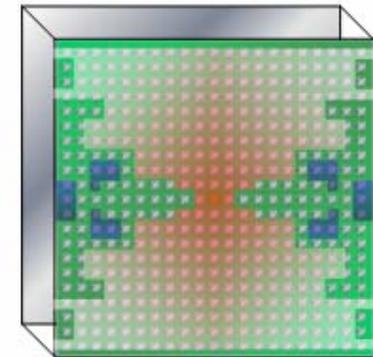
### • **18 Cell Silicon CMOS Process**

- Photovoltaic cell area 18 x 0.25 mm<sup>2</sup>
- Power received ~83  $\mu$ W
- $10^{17}$  n-doping photovoltaic cell (67 pF, ~30  $\mu$ A photocurrent @ ~0.5volts)
- Switching time ~ 1.2  $\mu$ s

## ESCAN Switch Design Considerations

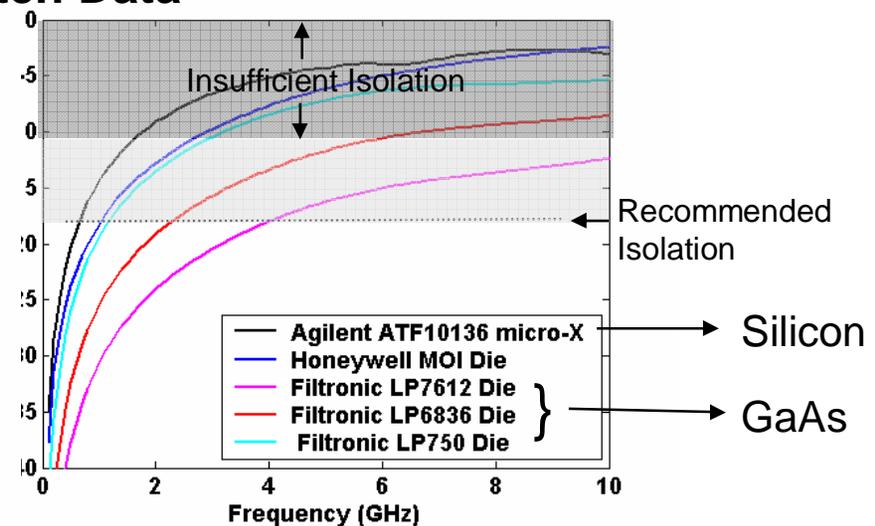
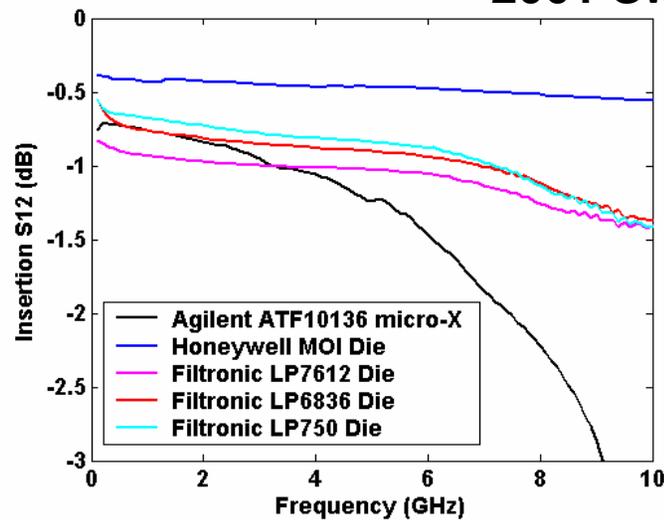
- Insertion loss (IL) and Isolation

- Low IL and high isolation designs diametrically oppose
- Insertion loss determines the physical extent of the element
- Increasing insertion loss gradually degrades the realized gain continuously (target <1 dB)
- Decreasing the isolation induces an abrupt change in the element performance (target < -11dB)



High Insertion Loss  
Currents attenuated at edges

### 2001 Switch Data

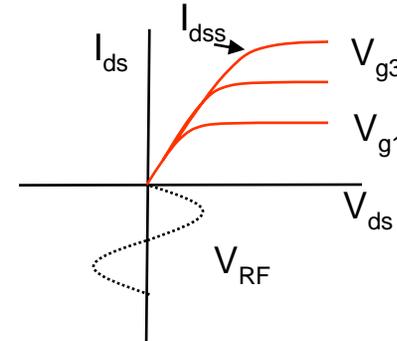


## ESCAN Power Handling Considerations

### • FET Power Handling

#### – ON State

- $I_{pk} > I_{DSS}$  compression results
- Max Power (On State)  $= 0.5 * (I_{dss\_max}^2 Z)$



#### – OFF State

- At RF frequencies  $V_g$  moves in sync with the RF swing on the drain (buys a factor of 2)
- Compression results when  $V_{RF}$  causes the  $V_{gd\_max}$  to be exceeded

$$V_{RF} = 2(V_{dg\_max} - V_g)$$

- When  $V_{RF}$  forces the FET beyond pinch off

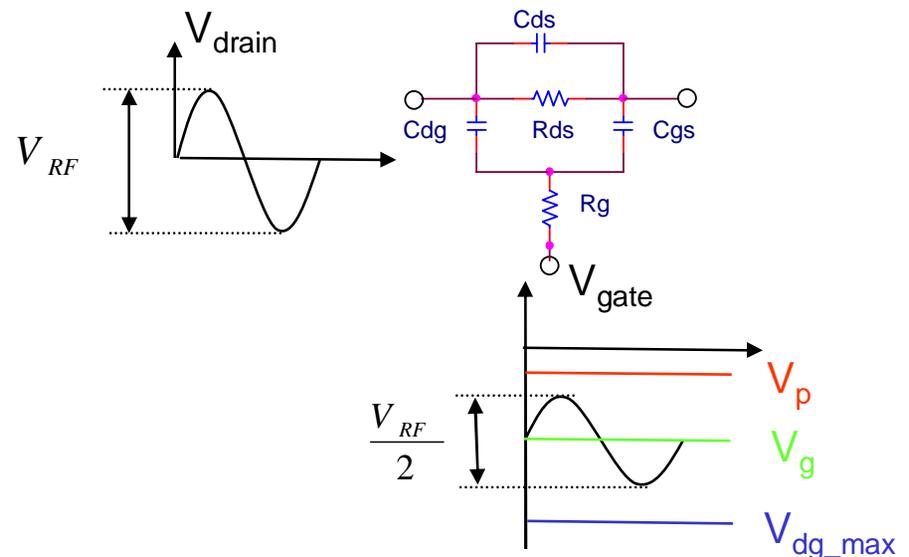
$$V_{RF} = 2(V_p - V_g)$$

- Optimum gate voltage

$$V_g = 0.5 * (V_p + V_{dg\_max})$$

- Max Power (Off State)

$$= 0.5 * (V_{dg\_max} - V_p)^2 / Z$$



## ESCAN Power Handling Estimates

- **FET Power Handling**

- **Typical Values**

- $V_{dg\_max} = -16$  V;
    - $V_p = -1.2$  V;
    - $V_{opt\_gate} = -8.6$  V;
    - $I_{dss} = 115$  mA @  $V_g = 0$
    - Utilizing a positive gate voltage to increase  $I_{dss}$  to  $I_{dssmax} \sim 1.5 * I_{dss} \sim 175$  mA
  - Max Power (Off State)  $\sim 2.2$ - $1.1$  Watt (for  $Z = 50\Omega$ - $100\Omega$ )
  - Max Power (On State)  $\sim 0.77$ - $1.53$  Watt (for  $Z = 50\Omega$ - $100\Omega$ )

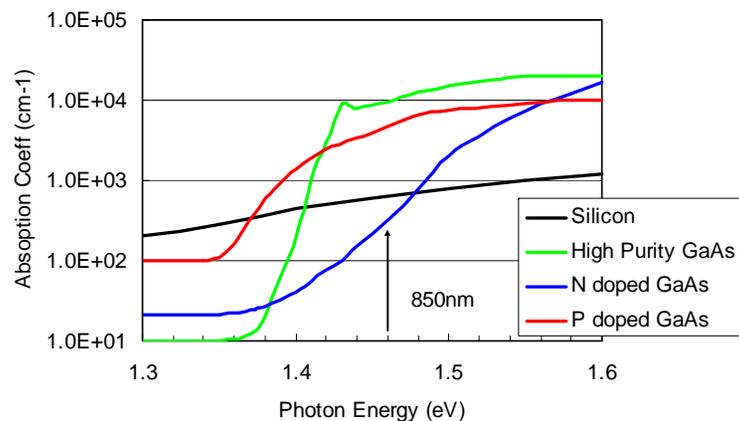
## ESCAN ASIC Process Selection Summary

### GaAs

- 850nm P-doped GaAs PD is most efficient
- Operation req. 11 ~0.9V Voc stacked PDs
- 300 micron FET switch has ~ 1.0 dB IL and 23 dB isolation at 2.4GHz
- GaAs substrates have low loss
- ESD protection is not required
- Logic not available
  - 2 ASICs & VCSELs per pad
- P doped GaAs is not readily available

### Silicon

- 850nm PD operation is less efficient
- Operation req. 18 ~0.5V Voc stacked PDs
- 300 micron NMOS SOI switches has ~ 1.0 dB IL and 19 dB isolation at 2.4GHz
- Si substrate degrades isolation and IL
- ESD protection req.
- CMOS logic circuits reduce VCSEL count
  - 1 ASIC & VCSEL per pad
- Process is readily available

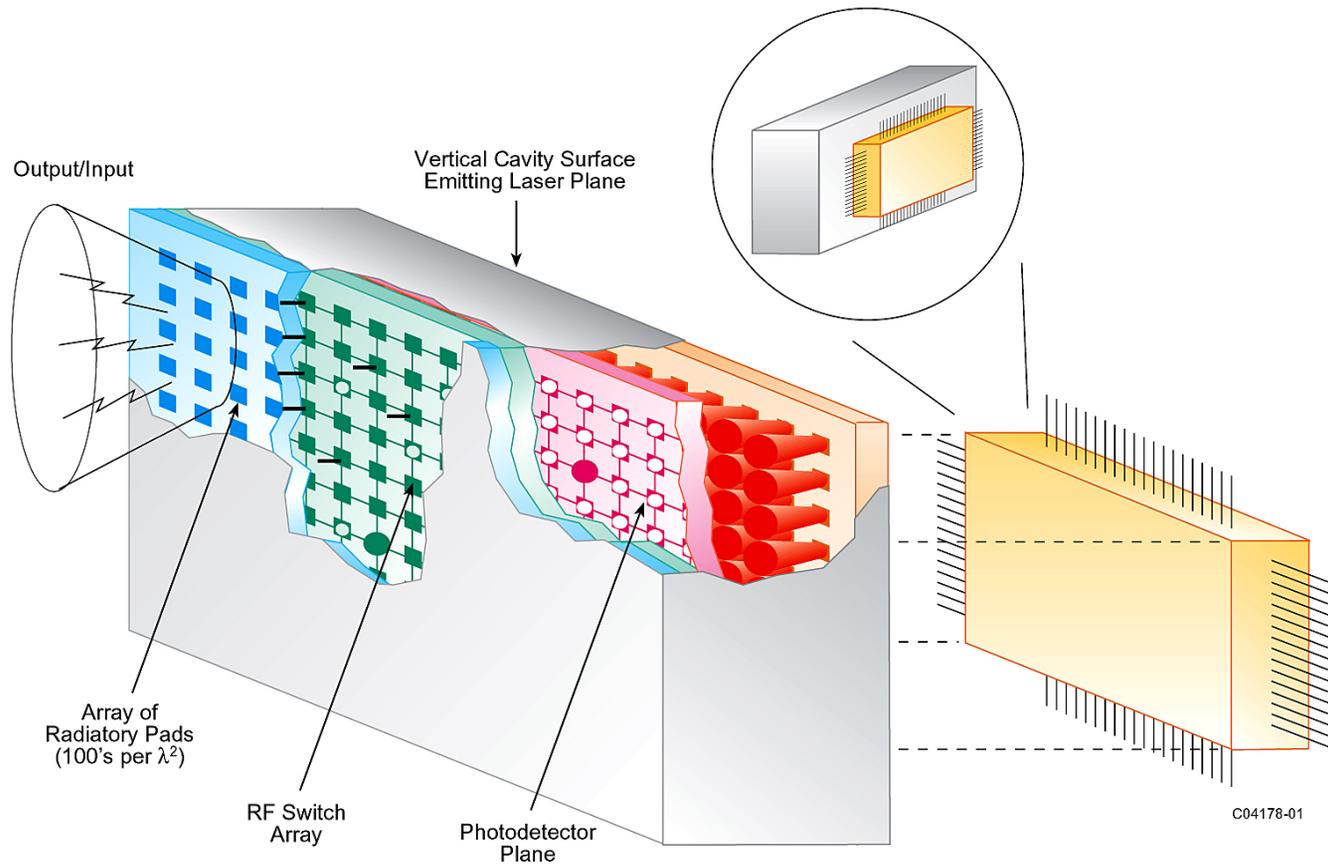


## Performance vs. Cost

## ESCAN: ASIC Process Summary

<b>GaAs Process</b>	<b>SOI Process</b>
Better Performance: <ol style="list-style-type: none"><li>1. Higher frequency capability</li><li>2. Lower performance risk</li></ol>	Lower Cost: <ol style="list-style-type: none"><li>1. Logic enables fewer VSCELS to be utilized</li><li>2. Process is readily available</li><li>3. Lower process risk</li></ol>

## ESCAN Integration



## ESCAN Measurement

ESCAN possess thousands of reconfiguration states posing a nontrivial measurement task.

Automated ground plane and range testing has been developed for these specialized apertures; for example at GTRI

